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# Impact of Guar Gum Derivatives on Properties of Freshly-Mixed Cement-Based Mortars

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## Abstract

Mortars are traditionally made from a mixture of sand, a binder and water. However, modern factory-made mortars are currently, very complex materials. Indeed, to exhibit various properties from the fresh paste to the hardened material, mortar formulations are composed of many mineral and organic admixtures. Among organic admixtures, polysaccharides, such as cellulose ethers (CE), are widely used into mortar formulation to improve water retention capacity of the freshly-mixed materials. The water retention capacity is an essential property of mortars leading to enhance the cement hydration and its adhesion to a substrate. Moreover, many polysaccharide admixtures, acting as viscosity-enhancing agents (VMA), prevent segregation and improve the homogeneity and workability of cement-based system. Indeed, the viscosity of the system strongly increases using polysaccharides and the rheological behavior of the cementitious paste may be completely modified and adapted to the application. Nevertheless, polysaccharides, as sugars, act on cement hydration. The main drawback is the retarding effect in hydration mechanism and setting-time of the cement.

The present study examines the influence of chemical composition and structure of guar gum derivatives on fresh state properties of Portland cement-based mortars, such as water retention capacity (WR) and rheological behavior of fresh state Portland-based mortars. This work focuses on the guar gum derivatives since their manufacturing process is low pollutant and they provide very good properties to cement-based mortars. The investigation was also completed by adsorption isotherms. For this purpose, a native guar gum, some HydroxyPropyl Guars (HPG) and some hydrophobically modified HPGs were selected. The effect of the molar substitution ( $MS_{HP}$ ) and the degree of substitution ( $DS_{AC}$ ) was investigated. The results highlight that chemical composition of HPGs has a remarkable effect on fresh state properties of mortars. The native guar gum does not impact both WR and rheological behavior. Increasing  $MS_{HP}$  leads to an improvement of the WR and the stability of mortars while the hydrophobic units further enhance WR and conduct to a decrease in the yield stress and an increase in the resistance to the flow of admixed mortars.

## Originality

Hydroxypropyl guars (HPGs) are very interesting molecules because they are able to induce water retention properties comparable to those obtained with cellulose ethers, which are the widely used water-retaining agent. Moreover, by adapting the chemical composition and structure of the Hydroxypropyl guars it is possible to improve the water retention capacity of mortars, to modify the rheological behavior of mortars and to decrease the impact of the admixtures on the hydration delay of cement. It is important to underline that manufacturing of HPG causes less pollution than cellulose derivatives. Therefore the use of HPGs is in fact already well-established in construction chemistry. Nevertheless, studies about HPG as admixtures for cementitious materials are very scarce in the published literature.

**Keywords:** Cement; HydroxyPropyl Guar; Mortar; Rheology; Water retention

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## 1. Introduction

Modern factory-made mortars are complex materials, in which several kinds of admixtures are added in order to obtain specific properties, from the fresh state to the hardened material. Indeed, since many years, concretes, mortars or cement grouts with high fluidity have been developed, since their use implies many economical and technical advantages. However, the use of highly flowable mixtures may lead to segregation or excessive bleeding and subsequently, durability issues. In order to overcome this problem by enhancing the sedimentation resistance while maintaining high fluidity, viscosity-enhancing admixtures (VEA) are frequently introduced within the formulation (Rols S. *et al.*, 1999; Khayat K. H. *et al.*, 1997; Lachemi M. *et al.*, 2004; Sonebi M., 2006). Among these admixtures, natural polysaccharides or their derivatives (such as welan gum, starch derivatives or cellulose ethers) are the most widely used. Moreover, the incorporation of these VEAs in shotcrete or render mortar is useful to ensure sagging resistance for thick application on vertical support, and to allow sufficient fluidity for normal pumpability by supplying shear thinning rheological behavior (Paiva H. *et al.*, 2006). Indeed, these admixtures provide, generally, high yield stress and apparent viscosity at low shear rate but low resistance to flow at high shear rate (Khayat K. H., 1998). However, their mode of action is not fully understood, since results are sometimes contradictory.

Water retention (WR) is another essential property of monolayer render at fresh state. Indeed, high water retention improves the cement hydration and limits the absorption of the mixing water by a substrate and thus provides good mechanical and adhesive properties to the mortar (Bertrand L. *et al.*, 2004; Jenni A. *et al.*, 2005). Among admixtures enhancing water retention capacity of the freshly-mixed mortars, cellulose ethers (CE) are the most widely used. Nevertheless, hydroxypropyl guar (HPG) are now also well-established in the construction industry as water retention agent for mortars (Biasotti B. *et al.*, 2011; Poinot T. *et al.*, 2013; Poinot T. *et al.*, 2014; Cappellari M. *et al.*, 2013). Moreover, HPGs are already widely used in various industrial fields, such as textile printing, hydraulic fracturing process, oil production or paper manufacturing, due to their thickening effect (Risica D. *et al.*, 2010; Lapasin R. *et al.*, 1995). Consequently, since HPGs improve the two main properties of mortar, they appear as suitable admixtures to be used in render formulation.

The aim of this study is to provide an understanding of the effect of chemical composition and structure of HPGs and its dosage on macroscopic properties of mortars. For this purpose, an original guar gum and five HPGs with specific chemical modifications, such as increase in MSHP or substitutions by hydrophobic units, were selected. The impact of admixtures on the water retention capacity and on the rheological behavior of mortars was investigated.

## 2. Materials and methods

### 2.1. Mineral products

Mineral products used in this study consist in blend Portland cement (Holcim), lime (Holcim), calcium carbonate (Calcitec V60, Mineraria Sacilese S.p.A.) and dolomite (Bombardieri and Leidi 0.1-0.4mm). The mineral compositions of the commercial Portland cement, CEM II/B-LL 32.5 R according to the European standard EN 197-1 (Standard EN 197-1, 2012), used are given in Tab. 1.

Tab. 1 Chemical compositions (% by weight) of the investigated cement determined by XRF and XRD-Rietveld refinement.

Compositions	CaO	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	MgO	Na <sub>2</sub> O	K <sub>2</sub> O	TiO <sub>2</sub>	SO <sub>3</sub>	LOI
Content (XRF)	57.9	12.3	5.2	4.0	1.2	1.0	1.7	0.2	4	13.7
Phase composition	C <sub>3</sub> S	C <sub>2</sub> S	C <sub>3</sub> A	C <sub>4</sub> AF	Calcite	Gypsum	Quartz	Free CaO		
Content (XRD + Rietveld)	54.3	3.5	4.7	4.6	28.9	3.0	0.9	0.8		

The phase composition was determined by Rietveld refinement method (Siroquant V2.5 software) after XRD analysis (D5000, Siemens) and the oxide composition was quantified by means of X-ray fluorescence spectroscopy. The median particle diameters by volume ( $d_{50\%}$ ) was determined by means of laser diffractometry with dry powder disperser (Mastersizer 2000 and Scirocco dispersing unit, Malvern) and the specific surface area (determined by BET) of all raw materials are given in Tab. 2.

Tab. 2 Median particle diameters by volume and specific surface area of the mineral phases.

	CEM II/B-LL	Lime	Dolomite Leidi	Dolomite Bombardieri	Calcite
$d_{50}$ ( $\mu\text{m}$ )	15	5	300	600	20
BET specific surface area ( $\text{m}^2/\text{g}$ )	2.40	5.67	0.43	0.34	1.44

## 2.2. Organic admixtures

Guar gum is a natural polysaccharide extracted from the seed endosperm of *Cyamopsis tetragonolobus*. This polymer consists in a  $\beta(1-4)$ -linked D-mannopyranose backbone with random branchpoints of galactose via an  $\alpha(1-6)$  linkage (Figure 1a). Hydroxypropyl guar (HPGs) are obtained from the original guar gum via an irreversible nucleophilic substitution, using propylene oxide in the presence of an alkaline catalyst (Figure 1b). The manufacture of HPGs has the advantage of having a more reduced impact on the environment than cellulose derivatives. Indeed, guar gum is extracted by simple thermo-mechanical process, exhibits a higher chemical reactivity and is soluble in cold water thanks to its branched-chain structure with a lot of hydroxyl groups. Thus, the chemical modification of the original guar gum requires normal reaction conditions of temperature and pressure, does not generate large quantity of by-products, and requires minimal purification procedure (Biasotti B. *et al.*, 2011).

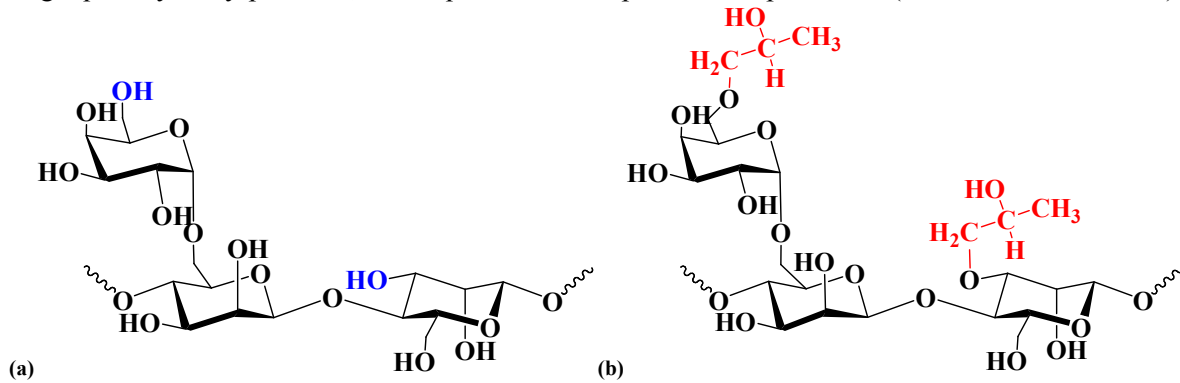


Figure 1 Molecular structure of original guar gum (a) and HydroxyPropyl Guar (b)

In this paper, three HPGs and an original guar gum provided by Lamberti S.p.A were studied. They exhibit roughly the same molecular weight, around  $2.10^6 \text{ g}\cdot\text{mol}^{-1}$  since they are all from the same original guar gum (noted HPG 6 in the paper) (Pointot T. *et al.*, 2013). Tab. 3 provides a qualitative description of the polymers used. The qualitative substitution degrees are provided by the manufacturers. The molar substitution ratio ( $\text{MS}_{\text{HP}}$ ) represents the number of hydroxypropyl units per anhydroglucose unit and is less than 3 for the investigated HPGs. The degree of substitution ( $\text{DS}_{\text{AC}}$ ) represents the amount of alkyl chain per anhydroglucose unit. The only difference between HPGs 1 and 3 is the molar substitution ratio, which increases, while HPG 4 exhibits an additional substitution (short alkyl chains).

Tab. 3 Qualitative description of the HPG used.

	$\text{MS}_{\text{HP}}$	$\text{DS}_{\text{AC}}$	Additional substitution
HPG 1	Low	-	-
HPG 3	High	-	-
HPG 4	High	Low	Short alkyl chain
HPG 6	-	-	-

## 2.3. Methodology

Mortars were prepared according to the following mixture proportions: 12% of cement, 3% of lime, 18% of calcium carbonate, 43% of dolomite Bombardieri and 24% of dolomite Leidi (by weight). The admixtures (0.05, 0.075, 0.1, 0.125 and 0.15%) were in addition to the total dry mixture (i.e. cement, lime, calcium carbonate and dolomite) and is expressed in weight percent by weight of binder (% bwob). Dry mixture was blended in a shaker (Wab, Turbula, Germany) for 10 min. Deionised water was added in order to obtain a liquid-to-solid ratio  $L/S = 0.22$ . The mixing procedure was in accordance with EN 196-1 (Standard EN 196-1, 2006).

The experimental methodology consisted in dividing the freshly mixed mortar into three parts in order to characterize several properties from the same mixing. A first part was used to characterize the rheological behavior of the mortar, the water retention study was performed on the second part and the third part of the freshly mixed mortar was centrifuged in order to determine the adsorption isotherms and the polymer concentration within the pore solution following a procedure described later.

In order to improve the understanding of the mechanism involved in Water Retention, additional dosages were tested for WR and adsorption measurements: 0.03 and 0.06% bwob for HPG 4, 0.06% bwob for HPG 3, 0.175 and 0.2% bwob in the case of HPG 1 and 0.2% bwob for the native guar gum (HPG 6).

All tests were carried out, at least, in triplicate and at a controlled temperature because water retention, rheological behavior of the mortar and adsorption isotherms are temperature-dependent. A control test was also performed with a mortar without admixture.

#### 2.4. Adsorption curves of HPGs into mortars

The adsorption isotherms were determined using the depletion method. The non-adsorbed polymer remaining within the pore solution was quantified by means of Total Organic Carbon (TOC) measurements. Prior to analysis, the pore solution was extracted from admixed or non-admixed mortar. The extraction was performed by means of two centrifugation steps. The first step consisted in the centrifugation of around 150 g of mortar at 5000 rpm for 5 min. The supernatant was, afterward, centrifuged again at 14500 rpm for 10 min in order to avoid the presence of mineral particles within the solution. The supernatant was diluted with hydrochloric acid solution at 0.1 mol.L<sup>-1</sup>. The total organic carbon was determined by combustion at 850 °C with a Vario-TOC Cube (Elementar). The adsorbed amount of polysaccharides was calculated from the difference of TOC content of the HPG reference solution and the TOC content of the supernatant.

#### 2.5. Water Retention of mortars

The water retention capacity of freshly-mixed mortar can be assessed using different tests where the removed water after suction or depression is measured (Paturl L. *et al.*, 2001). In this study, the standard method used to estimate the water retention capacity of a mortar, was the test described in ASTM C1506-09 and shown in figure 2 (Standard ASTM C1506-09, 2009).

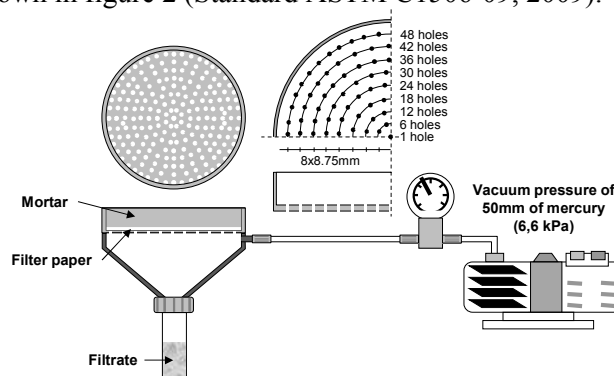


Figure 2 Device for Water Retention measurements

It had to be performed 15 min after mixing to measure the water loss of a mortar under depression. The standardized apparatus was submitted to a vacuum pressure of 50 mm of mercury (6.6 10<sup>3</sup> Pa) for 15 min. Then, the water retention capacity, WR, was calculated using the following equation:

$$WR(\%) = \frac{W_0 - W_1}{W_0} \times 100$$

where  $W_0$  represents the initial mass of mixing water;  $W_1$  is the loss of water mass after aspiration.

All the experiments were carried out at 20 °C. Three classes of water retention (measured by ASTM method) of a fresh mortar can be specified according to the DTU 26.1(Standard NF DTU 26.1, 2008.). The first class (low water retention category) contains mortars that exhibit water retention lower than 86%. The second class (intermediate) corresponds to values ranging from 86% to 94%. The last one (strong) is defined by water retention higher than 94%, corresponding to the required values in the field of rendering application.

## 2.6. Rheological behavior of mortars

The rheological measurements were performed with Rheometer MCR 302 (Anton-Paar), thermostated at 20 °C. The rheological properties of fresh mortars were investigated with vane-cylinder geometry (figure 3a) since this system is suitable for granular pastes like mortars (Bouras R. *et al.*, 2012; Barnes H. A. *et al.*, 2001). The gap thickness, distance between the periphery of the vane tool and the outer cylinder, was set at 8.5 mm, in order to be less sensitive to the heterogeneity of the mortar. Using a Couette analogy, the shear stress and shear rate were calculated from the torque and the applied rotational velocity respectively, after calibration with glycerol (Ait-Kadi A. *et al.*, 2002). The mortar was introduced into the measurement system at the end of the mixing cycle. At 10 min, the mortar was pre-sheared for 30 s at 100 s<sup>-1</sup> in order to re-homogenize the sample and to eliminate its shear history because of thixotropic character of cementitious materials (Phan T. H. *et al.*, 2006; Roussel N. *et al.*, 2012). After a period of rest of 5 min, the rheological measurements were started (total time = 15 min). At this time, the hydration rate is low enough which allows overcoming the irreversible effect of cement hydration on rheological behavior, especially at low shear rate (Phan T. H. *et al.*, 2006). The imposed shear rate was decreased by step from 300 to 0.06 s<sup>-1</sup> (16 steps). At each shear rate, the measuring time was adjusted in order to obtain a steady state whatever the formulation. The samples were systematically submitted to high shear rate (100 s<sup>-1</sup>) for 30 s before each imposed shear rate in order to resuspend particles of mortar within the mortar mixtures (figure 3b).

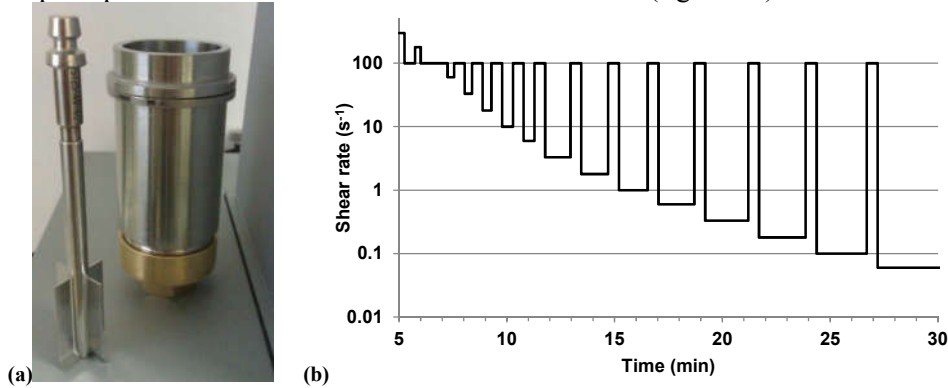


Figure 3 Experimental device (a) and experimental protocol for rheological measurements

The results were expressed as shear stress  $\tau$  according to shear rate  $\dot{\gamma}$  and the Herschel-Bulkley (HB) model was applied to fit the experimental data and used to describe mortars rheological behavior (Herschel W. M. *et al.*, 1926):

$$\tau = \tau_0 + K\dot{\gamma}^n$$

where  $\tau_0$  correspond to the yield stress, K the consistency coefficient and n the fluidity index.

## 3. Results and Discussion

### 3.1. Adsorption curves of HPGs into mortars

Figure 4 shows the adsorption isotherms of the hydroxypropyl guar and the original guar gum on Portland based-mortars. The results confirm that adsorption of original guar gum and HPGs on cementitious materials occurs. According to Wang *et al.* the adsorption mechanism of galactomannose polysaccharides at solid-liquid interfaces involves strong hydrogen bonding (Wang J. *et al.*, 2005). In the range of polymer dosage used in the present study, no plateau was reached, and this, whatever the admixture. For the original guar gum (HPG 6), the adsorption appears totally linear and is the highest of all the tested polymers, corresponding to a total adsorption higher than 98.5% of the introduced polymer.

The presence of hydroxypropyl substitutions on the guar leads to a decrease in the affinity of the polymer with the binder since the amount of HPG 1 adsorbed is lower than that of the original guar gum. The adsorption is further reduced by the increasing values of MS<sub>HP</sub> (HPG 3). This tendency is consistent with previous studies on HPGs and cellulose ethers (CE) (Pointot T. *et al.*, 2013; Brumaud C. *et al.*, 2014).

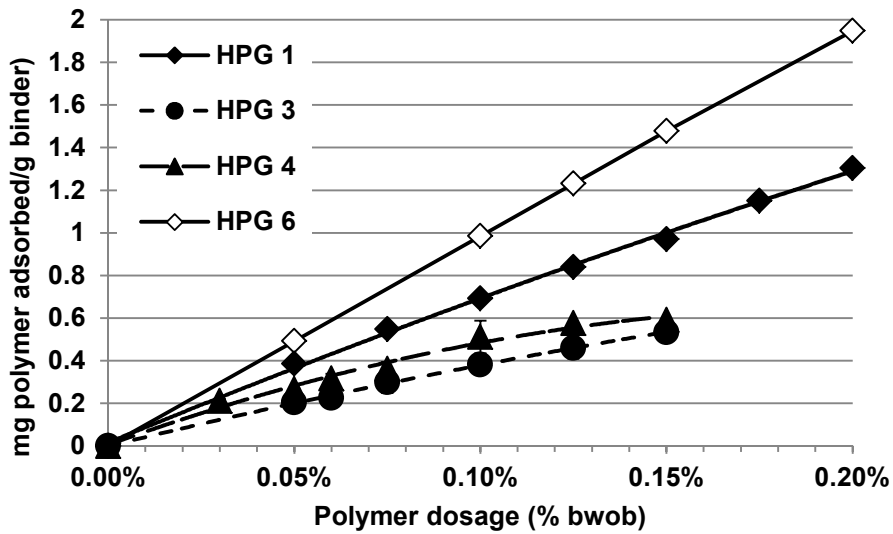


Figure 4 Adsorption isotherms of HPGs 1, 3, 4 and original guar gum (HPG 6)

Figure 4 highlights also the effect of the additional alkyl chain on the adsorption. It appears that the hydrophobic side chains slightly intensify the adsorption of the hydrophobically modified HPG on surface of grains with respect to HPG 3.

Consequently, the polymer concentration within the extracted pore solution rises following this order: HPG 6 < HPG 1 < HPG 4 < HPG 3. Excepted HPG 6, the amount of non-adsorbed polymer increases with increasing polymer dosage (results not shown here).

### 3.2. Impact of HPGs on the water retention property of fresh mortars

The evolution of the water retention capacity of fresh admixed mortars, according to the polymer dosage, is shown in figure 5. The non-admixed mortar exhibits a low water retention capacity of about  $72\% \pm 0.3\%$ .

The effect of the original guar gum (HPG 6) on the WR property seems negligible, regardless of dosage. This result is coherent with the adsorption of the polymer. Indeed, since the adsorption is higher than 98.5% of the initial amount of polymer, very few molecules are still in the pore solution (figure 4). The composition of pore solution is thus very close to that of the non-admixed mortar, leading to similar WR.

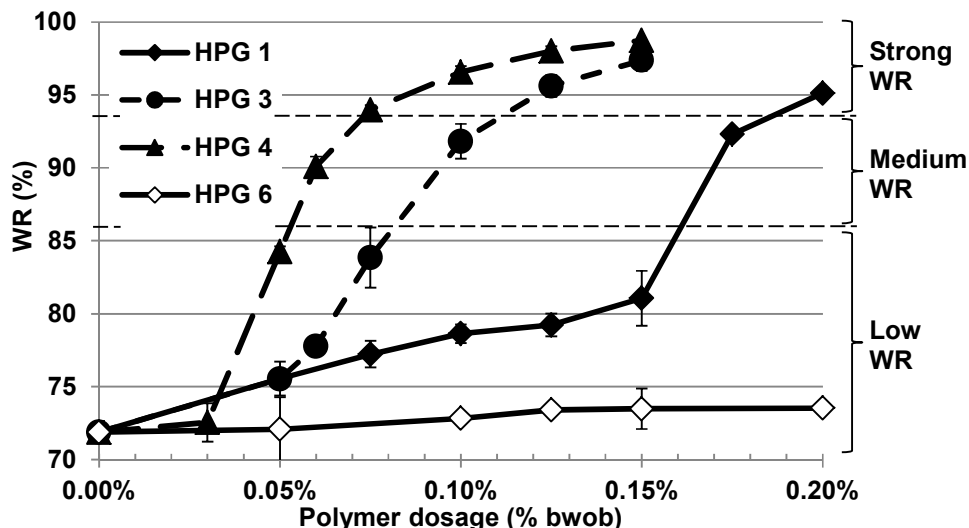


Figure 5 Impact of polymer dosage on water retention capacity of fresh admixed mortars

The water retention increases with the use of HPGs. Moreover, the WR rises according to polymer dosage, until reaching a plateau with very high WR values (>97%) for HPG 4. In the range of polymer dosage studied, the WR values reached for HPGs 1, 3 and 4 are greater than 94% and therefore belong

to the strong WR class. These results suggest that the substitution of hydroxyl units from original guar gum by hydroxypropyl units leads to an increase in WR of mortars. Furthermore, the increase in the  $MS_{HP}$  (from HPG 1 to 3) improves the WR capacity of mortar, since HPG 3 provides a higher WR despite a lower dosage. Moreover, an abrupt change in slope can be noticed for mortars admixed with HPGs 1 and 3. This occurs for a decreasing polymer dosage from HPG 1 to HPG 3. The results are consistent with those of previous studies performed with HPGs or CEs and with the proposed mechanism (Pointot T. *et al.*, 2014; Bülischen D. *et al.*, 2012; Marliere C. *et al.*, 2012). Indeed, the WR of admixed mortars is mainly governed by the ability of polysaccharidic admixtures to form a hydrocolloidal associated polymer molecules network and to induce overlapping of polymer coils within the pore solution (Pointot T. *et al.*, 2014; Bülischen D. *et al.*, 2012; Marliere C. *et al.*, 2012). When the concentration of polymer increases into the solution, the isolated polymer coils, existing at low polymer concentration, begin to come into contact each other. This concentration is defined as the coil-overlap concentration (noted  $C^*$ ). Above this critical concentration, the polysaccharide aggregates stop the water flow by plugging the porous network of a thin polysaccharide-enriched filter cake at the interface mortar-substrate resulting in a sudden and sharp rise in WR curves (Pointot T. *et al.*, 2014). The abrupt change in slope is reached for a decreasing polymer dosage from HPG 1 (0.15% bwob) to HPG 3 (0.05% bwob). The only difference between these HPGs is the increasing substitution degree. According to literature, the increase in  $MS_{HP}$  does not lead to a change in the  $C^*$  (Volpert E. *et al.*, 1996). However, the increasing substitution degree leads to a decrease in polymer adsorption on cementitious materials (figure 4) and hence an increase in polymer amount in pore solution. Consequently, the coil overlapping occurs at lower dosage.

The results furthermore highlight the positive impact of additional alkyl chain on WR. Indeed, the highest WR was obtained with HPG 4 for the lowest polymer dosages. Moreover, the abrupt change in slope occurs for a decreasing polymer dosage from HPG 3 (0.05% bwob) to HPG 4 (0.03% bwob). The presence of additional alkyl chains (HPG 4), despite slightly higher adsorption than HPG 3, leads to the formation of polymer associates at lower polymer dosage. Indeed, the interconnection between alkyl chains creates intramolecular and intermolecular interactions through specific hydrophobic interactions which cause a decrease in the coil-overlapping concentration (Cheng Y. *et al.*, 2002; Semenov A.N. *et al.*, 1995; Simon S. *et al.*, 2003). Consequently, the abrupt change in slope is reached for a lower polymer dosage of HPG 4 than HPG 3.

### 3.3. Rheological behavior of fresh mortars

The evolution of the yield stress, extracted from Herschel-Bulkley model, is shown in figure 6.

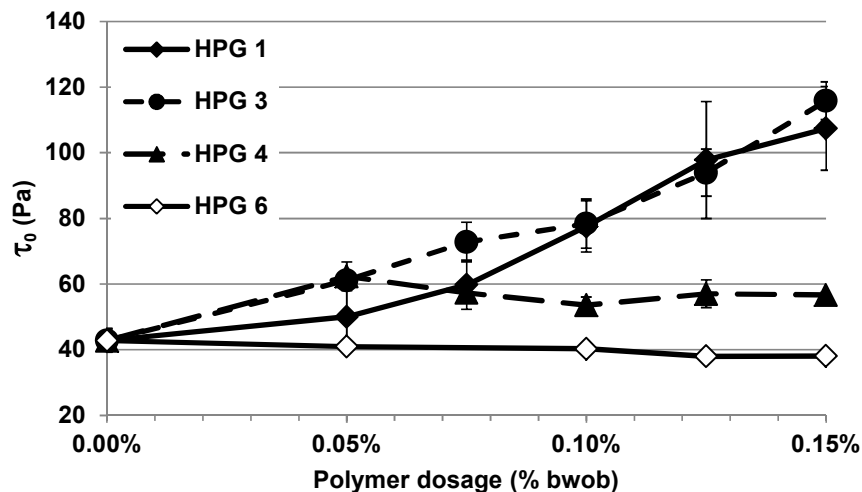


Figure 6 Impact of polymer dosage on yield stress of fresh admixed mortars (HPGs 1, 3, 4 and original guar gum (HPG 6))

The mortar without admixture exhibits a yield stress value of around 45 Pa. From the results, three classes of HPG, inducing different evolution of the yield stress with the polymer dosage, can be highlighted for admixed mortars. The first category only contains the original guar gum (HPG 6),



which induces a low and quasi linear decrease in the yield stress of mortar when HPG dosage increases. On the contrary, HPGs 1 and 3 lead to a continuous rise of the yield stress of mortars from 50-60 Pa to around 120 Pa with the increase in the HPG dosage from 0.05% to 0.15%. Finally, HPG 4 constitutes the third class of admixture. The use of this admixture leads an improvement of the yield stress compared to the non-admixed mortar, whatever the dosages tested in the study. However, the improvement is not proportional to the admixture dosage. Indeed, our first dosage (0.05% bwob) leads to a higher yield stress than non-admixed mortar. Beyond this dosage, increasing the dosage from 0.05% to 0.1% bwob provides a slow and low decrease in yield stress, before reaching a plateau for polymer dosages higher than 0.1% bwob. It is worth noting that the value of the yield stress reached on the plateau is still higher than that of the mortar without admixture.

Figure 7 presents the evolution of the consistency coefficient (K from Herschel-Bulkley equation). As in the case of the yield stress, the results can be divided into three classes of polymer. The first class is only composed of the original guar gum which provides a very low or negligible modification of the consistency coefficient with increasing polymer dosage compared to non-admixed mortar. HPGs 1 and 3, constituting the second group, induce first a low increase from in the consistency coefficient, followed by a plateau. Finally, HPG 4 leads to a continuous increase in the consistency coefficient of admixed mortars.

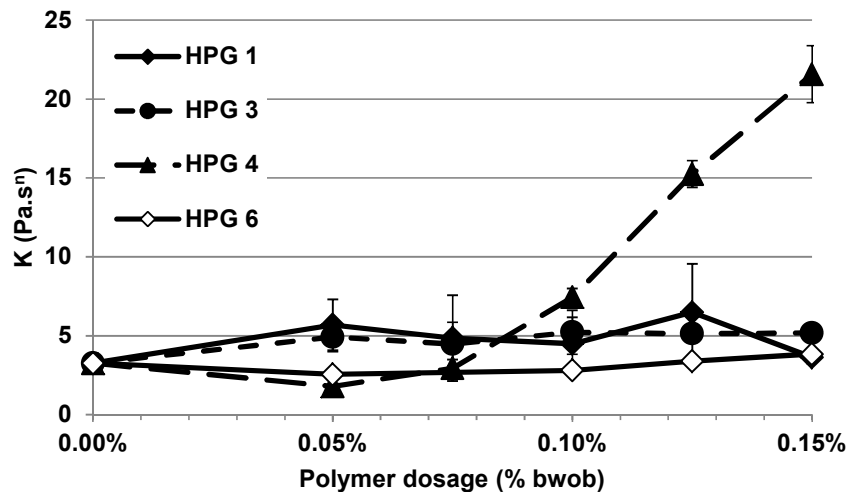


Figure 7 Impact of polymer dosage on consistency coefficient of fresh admixed mortars (HPGs 1, 3, 4 and original guar gum (HPG 6))

Figure 8 shows the evolution of the fluidity index (n) versus the polymer dosage for all the studied mortars. It is worth to note that whatever the mortars (non-admixed and admixed), the values of the fluidity index are lower than 1, meaning that they are all shear thinning. Due to the high standard deviation, the value of the fluidity index of mortars admixed with HPGs 1 and 3 and HPG 6 seem to be unchanged as the dosage of HPGs increase. However, HPG 4 leads to a low increase followed by a continuous decrease in the fluidity index until reaching values around 0.5. This means that the shear thinning behavior of mortars becomes more and more pronounced.

The rheological results (figures 6, 7 and 8) highlight that HPGs 1 and 3, HPG 4 and HPG 6 behave quite differently. Indeed, HPGs 1 to 3 lead to a continuous increase in the yield stress, while HPG 4 modifies mainly the consistency coefficient and the fluidity index. This means that HPGs 1-3 increase the stability of mortars while HPG 4 increases the resistance to the flow of admixed mortars. HPGs 1 and 3 affect the rheological behavior of the admixed mortars in the same way, i.e. an increase in the yield stress, a low increase followed by a plateau in the consistency coefficient and a negligible modification of the fluidity index when the polymer dosage rises. Figure 4 shows that HPGs adsorb onto particles constituting the mortar. Prima facie, this adsorption could be responsible for the increase in the yield stress because of bridging flocculation (Brumaud C. *et al.*, 2014). However, despite a strong drop of the adsorption (50%) with the increase in the  $MS_{HP}$  (from HPG 1 to 3) the yield stress also increases. This suggests that the non-adsorbed polymer may be responsible for the yield stress

increase. The potential loss of bridging can be compensated by an increase in the pore solution viscosity induced by the rise in the polymer concentration and/or by the depletion flocculation induced by the non-adsorbed coils (Palacios M. *et al.*, 2012). Moreover, the presence of HPG coils within the pore solution leads to an increase in the consistency coefficient (K) compared to non-admixed mortars. However, the expected increase in K due to the rise of pore solution viscosity with the polymer dosage can be compensated by steric hindrance, leading to a plateau for K.

Since the adsorption of original guar gum onto the surface of the binder is higher than 98.5%, one expects to detect a very strong increase in the yield stress compared to non-admixed mortar. However, the rheological behavior of the admixed mortar with the original guar gum is very close to that of the non-admixed mortar. This result suggests that the entire molecule of the original guar gum could be mainly adsorbed onto the surface of only one particle, limiting therefore the bridging flocculation. The very high concentration of free hydroxide groups on the backbone of the guar could be responsible of this mechanism. Moreover, the adsorption of the guar molecule onto a single particle leads to an increase in the steric hindrance and in the dispersion and lubrication effects, leading to a low but continuous decrease in the yield stress. For dosages higher than 0.1% bwob, the concentration in polymer coils (HPG 6) into the pore solution begins to slightly increase, leading to the beginning of the increase in the consistency coefficient and of the decrease in the fluidity index.

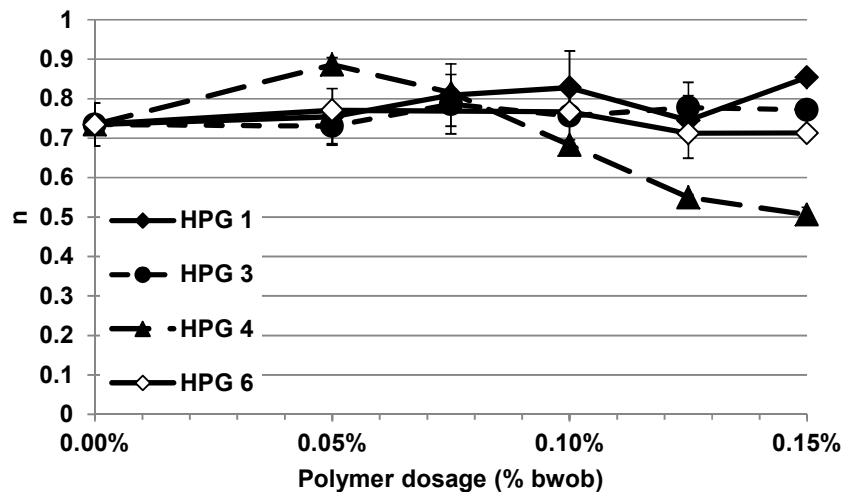


Figure 8 Impact of polymer dosage on fluidity index of fresh admixed mortars (HPGs 1, 3, 4 and original guar gum (HPG 6))

The additional alkyl chain also modifies the rheological properties of mortars. Contrary to HPG 3, HPG 4 leads to a strong and continuous increase in the consistency coefficient and a decrease in the fluidity index. These results highlight that mortars become more and more shear-thinning since the fluidity index decreases from 0.8 to 0.5. This rheological behavior gets more pronounced as the HPG dosage increases. These results are consistent with the fact that the hydrophobically modified HPG leads to the formation of coil overlapping at lower HPG dosage (between 0.03 and 0.05% bwob) since the presence of additional alkyl chains enhances the entanglement. Above this dosage, entanglement occurs between polymer coils, inducing a shear thinning behavior to the solution. At low shear rate, the entanglement of polymer coils leads to a higher pore solution viscosity and thus higher mortar viscosity. When the shear rate increases, the polysaccharide chains align in the direction of the flow resulting in less and less effect on mortar fluidity. The shear thinning behavior of the solution, and thus of the mortars, amplify with the increasing polymer dosage. The yield stress is also impacted by the additional alkyl chain. Indeed,  $\tau_0$  of mortar admixed with HPG 4, increases for a dosage equal to 0.05% bwob then slowly decreases for dosages ranging from 0.05% to 0.075% bwob, before reaching a plateau for higher dosages ( $\tau_0$  reached is still higher than that of the non-admixed mortar). This result could be explained by a change in the HPG conformation due to the presence of additional alkyl chains. Indeed, as previously mentioned, alkyl chain creates intramolecular and intermolecular

interactions through specific hydrophobic interactions. Intramolecular association of hydrophobic units tends to force the polymer chain into a more compact conformation (Simon S. et al., 2003; Aubry T. et al., 1994). Moreover, the conformation of hydrophobically modified polymers in aqueous solution involves the presence of alkyl chains mainly inside the coils in order to limit contacts between hydrophobic chains and water (Simon S. et al., 2003). Consequently, the hydrophilic groups, such as hydroxyl and hydroxypropyl, are preferentially on the outskirts of the coils, promoting the adsorption onto the surface of particles (figure 4) and therefore steric hindrance which implies a prevention of direct contacts between particles. Moreover, due to a more compact conformation and avoidance between water and hydrophobic units, the bridging ability of hydrophobically modified HPG should decrease. All these points should lead to a decrease in the yield stress.

#### 4. Conclusions

In this paper, we studied the effect of several guar gum derivatives on water retention property and rheological behavior of mortars. Based upon the results, it was found that the original guar gum was totally adsorbed onto particle surface, leading to a negligible modification of WR and rheological behavior with respect to the non-admixed mortar. Depending of the chemical structure of HPGs, it is possible to promote the water retention according to two different ways. First, by increasing the  $MS_{HP}$  of HPGs, the amount of adsorbed polymer drops, which leads to an increase in the HPG concentration within the pore solution and therefore to lower HPG dosage necessary to reach coil overlapping. Second, by enhancing overlapping, the hydrophobically modified HPGs improve the effectiveness of WR agent at low dosage. HPGs also modify the rheological behavior of the mortars. As in the case of WR, the hydrophobic characteristic of HPGs is the preponderant parameter. Indeed, it was shown that additional alkyl chain mainly leads to a more shear thinning behavior of the mortar and to a rise in the consistency coefficient, while classical HPGs strongly increases the yield stress.

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